



## Porous polymer composite separators with three-dimensional ion-selective nanochannels for high-performance Li–S batteries

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### ABSTRACT

Lithium-sulfur (Li–S) batteries have been regarded as one kind of the most attractive candidates for next-generation energy storage devices for their high theoretical energy density and fairly low cost. However, the “shuttle effect” caused by diffusion of soluble polysulfides and uncontrollable growth of lithium dendrite seriously deteriorate the long-term cycle stability and safety of Li–S batteries in practical applications. Herein, a highly porous polyvinyl alcohol (PVA)/sodium carboxymethyl cellulose (CMC) composite separator with three-dimensional ion-selective nanochannels has been successfully fabricated via a facile non-solvent induced separation method. The abundant negative –COO<sup>−</sup> groups inside the nanochannels can hinder the undesired polysulfides penetrating through the separator, but allow Li<sup>+</sup> transporting rapidly and induce uniform lithium stripping/plating. As a result, the Li–S battery using the porous PVA/CMC composite separator realizes stable cycling with a low decay rate of 0.045% per cycle over 500 cycles at 1 C. This work offers a feasible strategy to design advanced multifunctional Li–S battery separators.

### 1. Introduction

On account of the low cost, high theoretical specific capacity (1675 mAh g<sup>−1</sup>) and outstanding energy density (2600 Wh g<sup>−1</sup>), lithium-sulfur (Li–S) batteries have been considered as one kind of the most potential next-generation energy storage devices to replace the conventional Li-ion batteries in the applications of portable electronics and new energy vehicles [1–4]. Nevertheless, Li–S batteries are still subject to some severe issues including (1) “shuttle effect” caused by the dissolution and diffusion of polysulfides in the ether-based electrolyte, which directly leads to rapid capacity fading and inferior cycling life, (2) low conductivity and high interface impedance due to the insulation nature of sulfur and Li<sub>2</sub>S<sub>2</sub>/Li<sub>2</sub>S, and (3) dramatic structural destruction of metallic lithium anode resulted from the uncontrollable growth of lithium dendrite [5–7].

For the past few years, numerous research efforts have been put into

solving the aforementioned problems. At the cathode side, researchers generally focus on boosting the interactions between polysulfides and the functional groups of cathode materials, such as nanosized inorganic materials [8,9], functional organic macromolecules [10–12] or porous carbon-sulfur composites [13–15]. At the anode side, establishing a robust solid electrolyte interface [16,17] (SEI) or preparing lithium alloy [18] as anode materials are commonly adopted as effective strategies to protect lithium anode from corrosion of polysulfides and lithium dendrite growth. Although the researches of cathode and anode modifications have been widely used for Li–S batteries, the complicated procedures and high cost usually limit their commercialized applications [19]. The separator, which is a vital part in liquid electrolyte systems, has profound effects on the electrochemical performance and safety of Li–S batteries. Polyolefin films are commonly used for Li-ion batteries owing to their good mechanical strength and appropriate chemical stability. However, it has been noted that polysulfides can

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easily pass through the commercial polyolefin separators and react with the lithium anode, giving rise to undesirable parasitic reactions. Meanwhile, the problem of lithium dendrite growth is still unsolved. Furthermore, the low ionic conductivity, poor thermal stability and interfacial compatibility are significant problems decreasing the battery performance as well [20]. Therefore, it is an important target to develop new types of separators with characteristics of high-efficiency, facility and scalability for trapping polysulfides and transfer Li ions as well.

The development of cation-selective separators with enormous number of negative groups like  $-\text{SO}_3^-$  and  $-\text{COO}^-$  has been recognized as effective approaches to block polysulfides from migrating toward the lithium anode by electrostatic repulsion interactions [21,22]. Besides, the cation-selective separator can provide obstruction for the movement of lithium salt anions, so as to promote the transference number of  $\text{Li}^+$  [23]. For utilizing the advantages of negatively charged materials, a simple way is to construct a coating layer on the surface of polyolefin separators which works as the polysulfide shield. For example, Babu and co-workers prepared a permselective sulfonated poly(ether ether ketone) / Nafion coating separator to selectively allow  $\text{Li}^+$  passing nonetheless the polysulfides are rejected [24]. Song et al. used a photografting method to obtain a carboxyl modified commercial polypropylene (PP) separator, which achieves a very low capacity loss of only 0.074% at 0.5 C for every cycle [25]. However, these strategies not only suffer from inferior interfacial adhesions between the polyolefin substrate and coating layer, but also reduce the energy density.

Sodium carboxymethyl cellulose (CMC) is one of the most widely used polyelectrolyte cellulose derivatives for its low price. As an anionic polyelectrolyte, the plentiful negative charges of CMC are expected to retard the movement of polysulfides. However, cellulose and its derivatives are difficult to form porous membranes due to their poor mechanical properties such as severe brittleness, resulting in the degraded electrochemical performances [26]. Polyvinyl alcohol (PVA) is a considerable polymer to strengthen the porous membrane as skeleton owing to its wonderful film-forming performance, high mechanical strength and chemical stability [27,28]. Besides, the abundant hydroxyls can offer intense hydrogen bonding interactions between PVA and CMC, thus resulting in a physically cross-linked structure within the polymer chains to ensure the compatibility and additional strength of the separators.

Herein, PVA and CMC, which are both water-soluble, thermally stable, eco-friendly and low-cost, have been solution blended to prepare a highly porous PVA/CMC composite separator with three-dimensional (3D) nanochannels by the non-solvent induced phase separation (NIPS) method as illustrated in Fig. 1. The carboxylate groups of  $-\text{COO}^-$  are

uniformly distributed within the porous nanochannels to effectively prevent the migration of polysulfides. Secondly, the oxygen-containing  $-\text{COO}^-$  groups and  $-\text{OH}$  groups can simultaneously regulate the deposition of  $\text{Li}^+$  and promote  $\text{Li}^+$  transport, thus effectively inhibiting the growth of lithium dendrites. As a result, the Li-S battery assembled with PVA/CMC composite separator at an optimized CMC content demonstrates ultra-stable cycling performance with a good capacity retention of  $520.9 \text{ mAh g}^{-1}$  after 500 cycles at 1 C and an ideal rate capacity of  $523.6 \text{ mAh g}^{-1}$  at 5 C.

## 2. Results and discussion

### 2.1. Physical and chemical properties of PVA/CMC separators

As demonstrated in Fig. 1, the non-solvent induced phase separation method, with the advantages of easy scalability, morphological controllability, and diverse selections of materials [29], is chosen for constructing the 3D nanochannels in PVA/CMC composite separators. Besides, to achieve appropriate porous structure and pore size, different compositions of PVA/CMC blends have been applied. As shown in Fig. S1, colorless and transparent solutions without visible phase separation are prepared to obtain the composite separators with different PVA/CMC ratios, which are signed as PC5, PC10, PC15 and PC20, respectively. According to previous reports [30], the entirely miscible blending systems will induce the information of sponge-like pores rather than finger-like voids via delayed mixing process, which can result in better mechanical strength for practical applications. Moreover, with the increasing components that are more immiscible with the non-solvent, the solvent-nonsolvent exchange rate will be further decreased, resulting in the generation of smaller nanochannels. The overall change trend of the porous structure and specific pore size distribution of PVA/CMC composite separators are depicted by scanning electron microscopy (SEM) and capillary flow porometry (CFP) tests, respectively. As presented in Figs. 2 and S2, when the mass ratio of CMC is lower than 5 wt%, the porous structure is irregular and cracks are visible on the top surface of PC5 (Fig. 2a) with partial non-porous areas. With the increasing content of CMC, the pores become smaller and uniform, accompanying with the compact sponge-like structure in the cross-sectional views (Fig. 2f-h), indicating that 3D nanochannels are built up by increasing the CMC content. CFP results confirm that the PVA/CMC composite separators with more CMC content possess smaller pore size (Fig. 2i-l). Hansen solubility parameter (HSP) is generally used to calculate the affinity between different materials. HSP includes the following three parts: a dispersion force component ( $\delta_d$ ), a polar

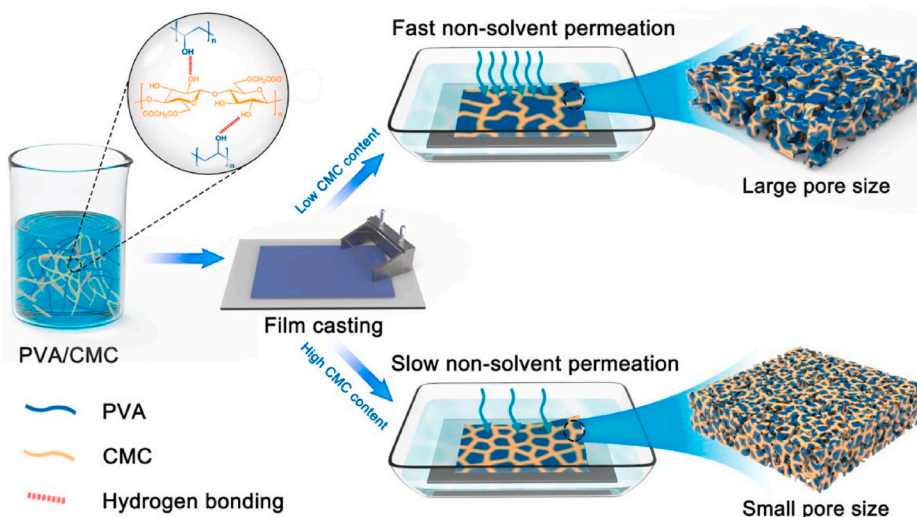


Fig. 1. The schematic illustration of the PVA/CMC composite separators.

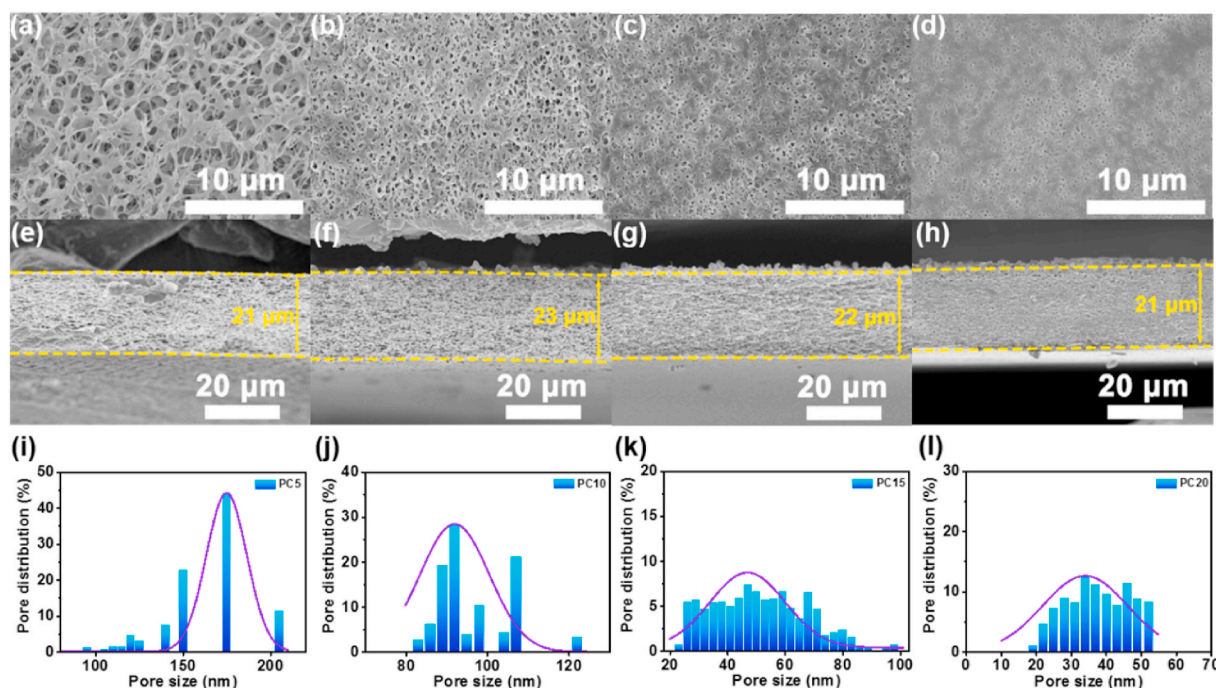


Fig. 2. The top-view and cross-view SEM images of (a, e) PC5, (b, f) PC10, (c, g) PC15 and (d, h) PC20 separators, respectively. (i–l) The corresponding pore size distributions of different separators.

component ( $\delta_p$ ), and a hydrogen bonding component ( $\delta_h$ ). In order to determine the solubility of a polymer in an organic solvent, HSP is calculated according to equation (1). Table S1 shows that the value of CMC-ethanol pair is larger than that of PVA-ethanol pair, which indicates that CMC is more immiscible with ethanol. Moreover, the incorporation of CMC results in higher viscosity of the polymer solution and stronger micro-crosslinking networks. Thus, the diffusion rate of ethanol into water is further decreased by the above factors, leading to the significant pore size reduction of PVA/CMC composite separators.

Porosity is an important parameter to evaluate the performance of separators. Herein, the porosity is tested by weighing the PVA/CMC composite separators before and after immersing in n-butanol as equation (2). It can be observed from Table S2, with the CMC concentration increasing from 5 wt% to 10 wt%, the porosity of PVA/CMC separators firstly increases from 54.5% to 63.3% due to the information of 3D nanochannels. Then, resulted from the gradual densification of the porous structure, it decreases to 48.8% when the CMC content is further increased to 20 wt%, but still being higher than that (40.3%) of the PP separator. Due to the low surface energy and hydrophobic characteristics, the compatibility between PP separator and conventional liquid electrolyte is essentially poor. As verified by the contact angle measurements in Fig. S3, the PP separator exhibits poor wettability to electrolyte with an inferior contact angle of 50.5°. In contrast, all the PC5, PC10, PC15 and PC20 separators can be readily wetted by electrolyte with the contact angles of 10.5°, 8.6°, 9.0° and 16.9°, respectively. To further investigate the electrolyte affinity of PVA/CMC composite separators, the electrolyte uptake and retention properties are obtained. As shown in Fig. S4a, the electrolyte uptake value of PC15 is the highest after 50 min, while the electrolyte retention value of PC20 is much superior. It's worth noting that the electrolyte absorbed by PP separator completely evaporates but still remains in all of PVA/CMC separators after 400 min (Fig. S4b), confirming that PVA/CMC composite separators can accelerate the permeation of electrolyte and ensure the good contact between electrolyte and electrode.

The thermal stability of separators is another concern regarding battery safety performance. Fig. S5a shows the thermogravimetric analysis (TGA) curves of PVA, CMC and PVA/CMC composite

separators. The pristine PVA exhibits inferior thermal stability with a low decomposition temperature at 230 °C, whereas the separators incorporated with CMC show much higher decomposition temperature compared to that of pure PVA. The optical images of PVA/CMC and PP separators before and after heating at 170 °C are shown in Fig. S5b. Obviously, the negligible thermal shrinkage with almost no shape change confirms the excellent thermal stability of PVA/CMC separators, as compared to the PP separator which is melt and suffers severe dimensional shrinkage under the same condition. The thermal behavior of the composite separators, are further depicted by differential scanning calorimeter (DSC) analysis (Fig. S6). There are one narrow and one broad endothermic peak for pristine PVA respectively, corresponding to the melting phase transition and glass transition at 87 °C. On the other hand, CMC exhibits a broad endothermic peak referring to the overlapping  $T_g$  and  $T_m$  of its semi-crystalline nature [31]. The glass transition position of PVA/CMC composite separators is turned into a broad endothermic peak and moves toward the low temperature region, which demonstrates the decreased crystallinity, good compatibility and hydrogen bonding interactions between PVA and CMC [32–34].

X-ray diffractometer (XRD) patterns further manifests the transformation of crystallinity with different CMC contents (Fig. S7a). A broad diffraction peak appears at  $2\theta = 20.2^\circ$  for CMC while PVA has a sharp diffraction peak at  $2\theta = 19.8^\circ$  with two broad diffraction peaks at  $2\theta = 22.4^\circ$  and  $40.8^\circ$ . On the other hand, the PVA/CMC composite separators show similar crystal structure with two broad diffraction peaks at  $2\theta = 19.0^\circ$  and  $22.3^\circ$ . The increased amorphous region of PVA/CMC composite separators indicates that the addition of CMC greatly reduces the crystallinity of PVA/CMC composites, which may provide a better ionic conductivity for lithium batteries [35]. Fourier transform infrared (FTIR) spectra demonstrates the intermolecular hydrogen bonding interactions between PVA and CMC (Fig. S7b). The pure CMC shows a broad strong band appearing at  $3428\text{ cm}^{-1}$  which is assigned to the  $-\text{OH}$  stretching vibration, while the asymmetric stretching vibration of  $-\text{C}=\text{O}$  is observed at  $1646\text{ cm}^{-1}$ . For PVA/CMC composites, both of the  $-\text{OH}$  and  $-\text{C}=\text{O}$  characteristic peaks are shift into lower wavenumbers, indicating that the composites are affected by the intermolecular hydrogen bonding interaction which reduces the force constants



of –OH and –C=O groups [33,36].

A mechanically robust separator can undergo high tension after casual collisions and reduce the possibility of internal short-circuits caused by the rough electrode surface and growth of lithium dendrite. To evaluate the mechanical strength of PVA/CMC composite separators, stress-strain curves are depicted in Fig. S8a. It is clearly demonstrated that the introduction of a certain amount of CMC has positive effects on the strength of the composite separators. The commercial PP separator presents an obvious orientation with a minimal tensile strength of 13.5 MPa and Young's modulus of 340 MPa at one direction, and a maximum tensile strength of 84.9 MPa and Young's modulus of 808.0 MPa at the other direction. The tensile strength of PVA, PC5, PC10 and PC15 separators are 4.20, 11.4, 15.4 and 21.2 MPa, respectively, with the corresponding Young's modulus of 259, 284, 384 and 889 MPa. However, the tensile strength and Young's modulus of PC20 decrease to 16.7 MPa and 883 MPa, which is resulted from the poor mechanical property of CMC. Nonetheless, the tensile strength of PC20 separator is not inferior to PP and PVA separators. Benefitting from the amorphous phase structure, the elongation at break of PVA/CMC composite separators are all much higher than that of PP separator except for PC20 separator, which is crucial to resist the penetration of lithium dendrite [37].

In order to verify the efficiency of polysulfide obstruction by the

PVA/CMC composite separators, polysulfide permeation tests are conducted as shown in Fig. 3a. The PC15 separator is selected as the experimental group because of its suitable porous structure and sufficient mechanical strength. To be noticed, at a relatively high polysulfide concentration, the polysulfides easily diffuse across the separator into the originally colorless blank electrolyte in the opposite chamber with PP separator even at 0 h. Conversely, the PC15 separator shows a much slower polysulfide permeation rate with almost invisible color change of the blank electrolyte after 24 h. The UV-vis test of the electrolyte obtained at each point-in-time further verifies the very low absorbance intensity of diverse polysulfides in electrolyte after 8 h by using PC15 separator (Fig. 3b), demonstrating efficiently inhibited polysulfide diffusion by the coulombic interactions between –COO<sup>-</sup> groups and polysulfide anions within the 3D nanochannels as illustrated in Fig. 3c.

## 2.2. Electrochemical properties of PVA/CMC composite separators

Cyclic voltammetry (CV) profiles for the batteries assembled with PP and PC15 separators are presented in Fig. 4. Two reduction peaks can be clearly observed at about 2.3 V and 2.0 V, which represent the transformation of elemental sulfur to long-chain polysulfides ( $\text{Li}_2\text{S}_n$ ,  $4 < n < 8$ ) and soluble polysulfides to solid lithium sulfides ( $\text{Li}_2\text{S}_2/\text{Li}_2\text{S}$ ),

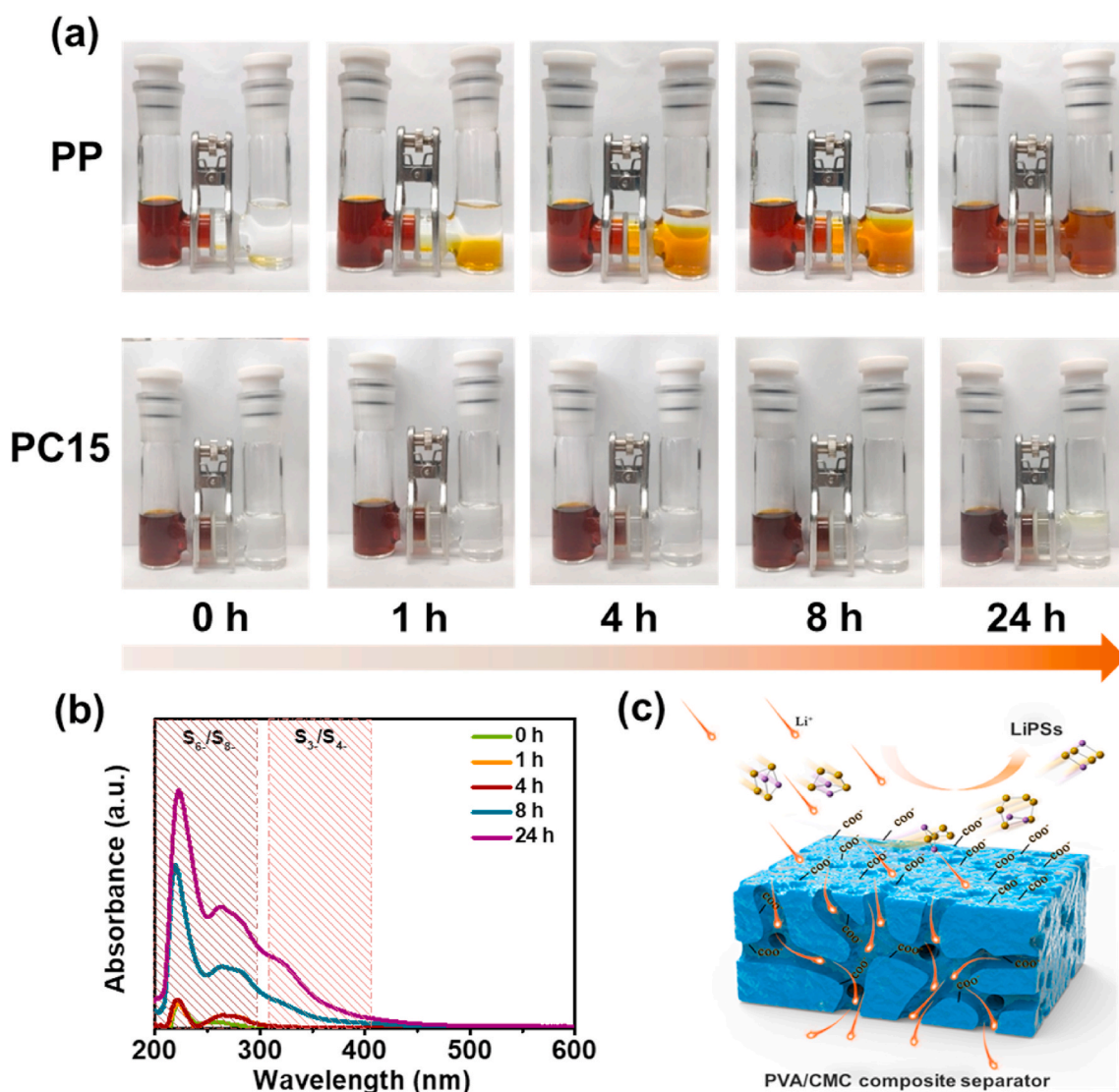
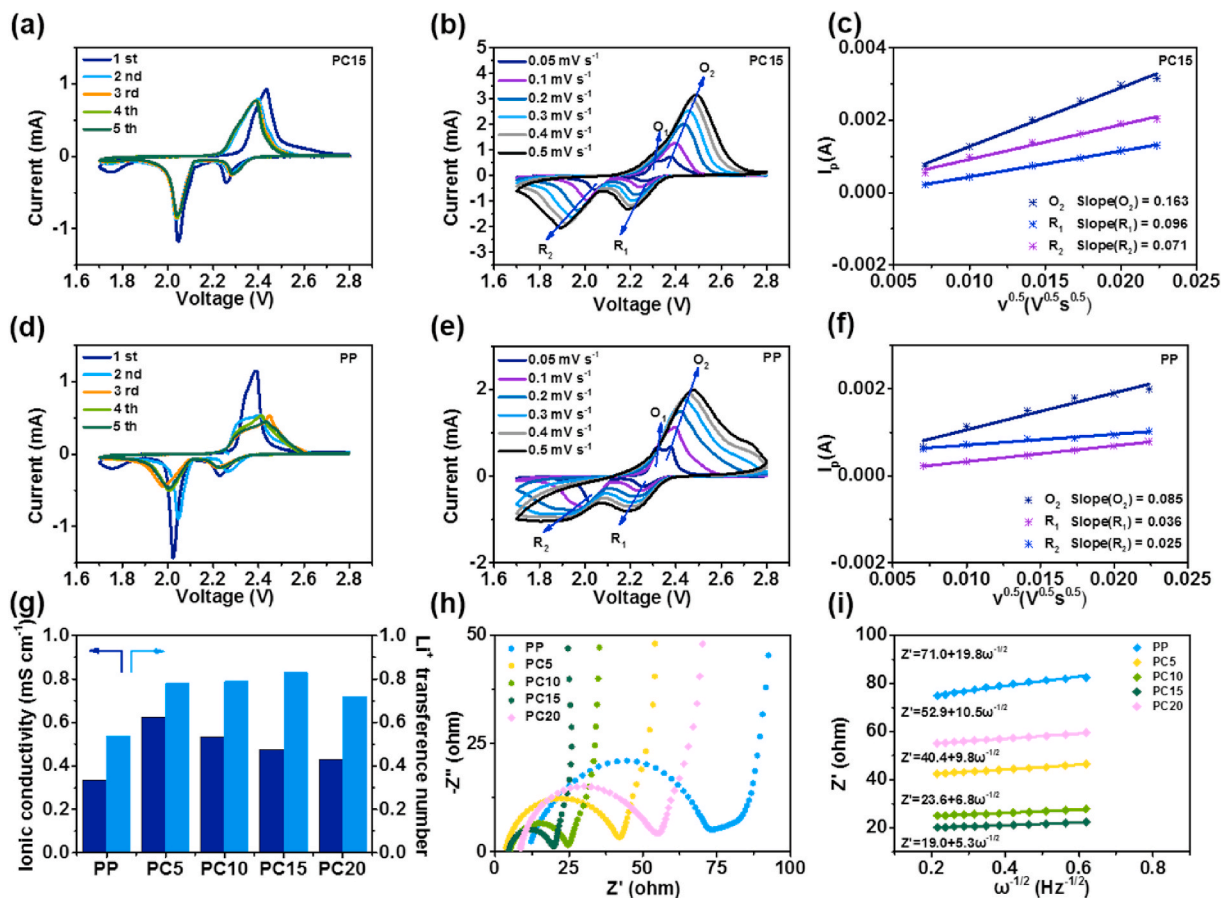


Fig. 3. (a) Polysulfide permeation measurements of PP and PC15 separators at varied time. (b) UV-vis spectra of pure electrolyte solution within electrolytic tank of PC15 separator in each point-in-time. (c) Illustration of polysulfide rejection by the 3D ion-selective nanochannels of PVA/CMC composite separators.



**Fig. 4.** (a, d) CV curves of the first five cycles, (b, e) CV curves at various voltage scan rates, and (c, f) the corresponding linear fits of the peak currents in each voltage scan rate of PP and PC15 separators. (g) Ionic conductivity and lithium transference number, (h) Nyquist plots, and (i) Relationship between  $Z'$  and  $\omega^{-1/2}$  in the low-frequency region in EIS test of PP, PC5, PC10, PC15 and PC20 separators, respectively.

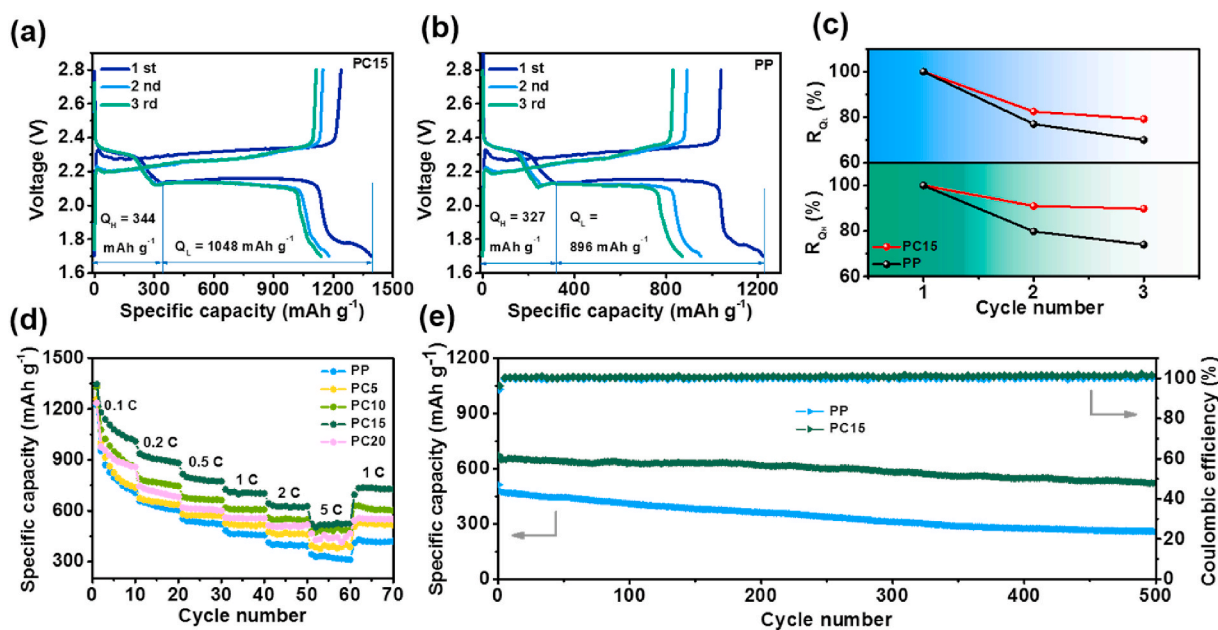
respectively [38]. In the part of anodic scan, an overlapping oxidation peak appears at about 2.5 V, which is associated with the conversion of different polysulfide species into elemental sulfur. Meanwhile, the weak peak around 1.75 V is attributed to the reaction of  $\text{LiNO}_3$  in the initial cycle [39]. Impressively, the cell with PC15 separator exhibits lower voltage gap than those of PP separator, indicating that the PC15 separator can reduce polarization and provide better stability and reversibility for Li-S batteries [39]. Furthermore, with the increase of scan rate, the oxidation peaks of the cell with PC15 separator shift to higher potentials while the reduction peaks shift to lower potentials in Fig. 4b. However, the cell with PP separator suffers from severe polarization on account of the slow reaction kinetics (Fig. 4e). The  $\text{Li}^+$  diffusion coefficients ( $D_{\text{Li}^+}$ ) of the separators are also calculated by fitting the peak current of the CV curves with different scan rates by Randles-Sevcik equation [40,41]. As shown in Fig. 4c and f, the slope of each fitting curve for cells with PC15 are all higher than those of the cells with PP separator, revealing a higher  $D_{\text{Li}^+}$  value. Besides, the  $D_{\text{Li}^+}$  values of other cells with PC5, PC10 and PC20 separators are all higher than that with PP separator (Fig. S9), demonstrating the 3D nanochannels can facilitate  $\text{Li}^+$  transfer.

To further investigate the ionic conductivity, Nyquist plots of the separators are shown in Fig. S10, which present straight lines in the high frequency region. The ionic conductivity of PC5, PC10, PC15 and PC20 separators are obtained from  $Z'$ -intercept according to the extrapolation method which reach 0.62, 0.54, 0.48 and 0.43  $\text{mS cm}^{-1}$  respectively, being much higher than that (0.33  $\text{mS cm}^{-1}$ ) of PP separator (Fig. 4g). Furthermore, the  $\text{Li}^+$  transference number of PC5, PC10, PC15 and PC20 separators are 0.78, 0.79, 0.83 and 0.72 respectively (Figs. 4g and S11), being much higher than that (0.54) of PP separator. The above results

strongly prove that the introduction of  $-\text{COO}^-$  groups can improve the transfer ability of  $\text{Li}^+$ , thus effectively inhibiting the growth of lithium dendrite according to the Chazalviel's model [42,43].

In the Li-S batteries, the interfacial property plays the key role in the electrochemical performance. As shown in Fig. 4h, the bulk resistances ( $R_b$ ) of the cells with PC5, PC10, PC15 and PC20 separators before cycling are only 3.0, 5.0, 4.6 and 8.0  $\Omega$ , respectively, which are all significantly lower than that (11.1  $\Omega$ ) of PP separator. Additionally, the cells assembled with PC5, PC10, PC15 and PC20 separators present quite low interfacial resistance ( $R_{ct}$ ) of 42.9, 19.1, 14.7 and 45.3  $\Omega$ , respectively. Compared to the  $R_{ct}$  (61.6  $\Omega$ ) of PP separator, the dramatically reduced semicircle part suggests that the interfacial ion transfer of the cells are faster when PVA/CMC composite separators are used. Besides, the  $\text{Li}^+$  diffusion coefficients of PVA/CMC composite separators calculated by equation (5) are well matched with the  $\text{Li}^+$  diffusion coefficients calculated by CV curves (Fig. 4i and Table S4), which further verify that the polar functional  $-\text{COO}^-$  can facilitate  $\text{Li}^+$  transport [44].

Galvanostatic charge-discharge tests of the Li-S batteries are firstly carried out at 0.1 C. As shown in Fig. 5a-c, owing to the satisfactory interfacial contact and attenuated polarization, the cell with PC15 separator delivers a high initial capacity of 1392  $\text{mAh g}^{-1}$ , which is consisted of a short and high plateau ( $Q_H = 344 \text{mAh g}^{-1}$ ) as well as a long and low plateau ( $Q_L = 1048 \text{mAh g}^{-1}$ ) corresponding to the two reduction peaks in CV curves, and being higher than those of PP separator ( $Q_H = 327 \text{mAh g}^{-1}$ ,  $Q_L = 896 \text{mAh g}^{-1}$ ). Besides, the relatively high capacity retention of the cell with PC15 separator in the first three cycles suggests the efficient suppression of polysulfide permeation during the cycles. The rate performance is an important criterion in the assessment of electrochemical performance of Li-S batteries. As



**Fig. 5.** The first three charge/discharge voltage curves for cells with (a) PC15 separator, (b) PP separator and (c)  $R_{QH}$  and  $R_{QL}$  of the cells with PP and PC15 separators, respectively. (d) Rate performance for cells with different separators at various current rates. (e) Galvanostatic cycling performance at 1 C for cells with PP and PC15 separators.

presented in Fig. 5d, at different scan rates of 0.1, 0.2, 0.5, 1, 2 and 5 C, the specific capacities of the cells with PVA/CMC separators are all much higher than that of PP separator. Especially, the cell with PC15 separator reaches the high specific capacities of 711.8, 624.4 and 523.6  $\text{mAh g}^{-1}$  at 1, 2 and 5 C, respectively. Furthermore, after the high current density cycling at 5 C, the cell with PC15 separator recovers to 736.2  $\text{mAh g}^{-1}$  at the following 1 C cycling, manifesting that PC15 separator can endow the Li-S battery with outstanding reversibility. Besides, resulting from the decreased interfacial resistance and faster  $\text{Li}^+$  transport, the over potential of the cell with PC15 separator at 5 C is 480 mV (Fig. S12a), being dramatically lower than that (638 mV) of PP separator (Fig. S12b).

Fig. S12c reveals the cycling performance of the cells with diverse separators at a low current density of 0.2 C. After 200 cycles, the cells with PP, PC5, PC10, PC15 and PC20 separators maintain the capacity of 322.5, 485.2, 643.9, 466.2 and 252.2  $\text{mAh g}^{-1}$ , respectively. Particularly, the enhanced rejection ability of PVA/CMC separators toward polysulfides appears only in the CMC content range of 5–15 wt%, which can be attributed to the decreased pore size and increased  $-\text{COO}^-$  content of the separators. For the cells with PC20 separator, even though the pore size fairly decreases, the poor mechanical strength may cause the destruction of porous structure in the cycling process and result in the undesired capacity fading. In the long-term cycle at 1 C, a remarkably low specific capacity attenuation rate of 0.045% per cycle is observed for the cell with PC15 separator with a high specific capacity of 520.9  $\text{mAh g}^{-1}$  and a high coulombic efficiency ( $>99.1\%$ ) after 500 cycles, which is evidently much better than other previously reported studies (Table S5). By contrast, the cell with PP separator only maintains a low capacity of 259.4  $\text{mAh g}^{-1}$ , further demonstrating that the negative  $-\text{COO}^-$  groups on the surface of the well-tailored 3D ion-selective nanochannels can efficiently suppress the shuttle effect of polysulfides.

After 100 cycles at 1 C, the morphology of lithium anode is examined by SEM. The lithium surface of the cell with PC15 keeps smooth and integrity, indicating that polysulfides are confined to the cathode side (Fig. S13a). In sharp contrast, the lithium surface of the cell with PP separator is acutely corroded by polysulfides (Fig. S13b) compared to the pristine lithium anode (Fig. S13c). EDS mapping results demonstrate that almost no sulfur signal is found on the lithium anode surface for the

cell with PC15 separator, whereas  $\text{Li}_2\text{S}$  deposits on the lithium anode surface in the cell with PP separator, indicating that the 3D ion-selective nanochannels can serve as a strong polysulfide barrier. Fig. S14 further shows the morphology of PC15 separator after cycling. The porous structure remains intact while the anode side of the separator keeps its pristine color without any deposition of polysulfides, proving the excellent stability of the PVA/CMC separator during long-term cycling process. To further investigate the suppressing effect of lithium dendrite growth with PC15 separator, the long-term galvanostatic cycling test with symmetrical cells of  $\text{Li}/\text{separator}/\text{Li}$  is carried out at various current densities. As shown in Figs. S15a and S15b, benefiting from the high  $\text{Li}^+$  transfer and lithiophilic groups [45,46], the symmetric cell with PC15 separator displays a relatively low overpotential and outstanding stability at the current density of 1 and 2  $\text{mA cm}^{-2}$ . On the contrary, the overpotential of the cell with PP separator continuously increases, which can be explained by the severe electrolyte decomposition during the lithium dendrite growth process [47,48]. Fig. S15c shows that at different current densities of 0.5, 1, 2 and 5  $\text{mA cm}^{-2}$  with a constant capacity of 1  $\text{mAh cm}^{-2}$ , the cell with PC15 separator still maintains a low overpotential without voltage fluctuation, especially at high current densities. This is also consistent with the smooth, uniform and compact morphology of the lithium anode of the cell with PC15 separator as shown in Fig. S16a. However, the lithium anode is covered with mossy-like and nodule-like lithium dendrites with PP separator (Fig. S16b). Therefore, the PVA/CMC composite separators can play a crucial part in obstructing shuttle effect and suppressing lithium dendrite for high-performance Li-S battery applications.

### 3. Conclusions

In summary, 3D ion-selective nanochannels have been constructed in the PVA/CMC composite separators for simultaneous polysulfide rejection and lithium dendrite suppression via NIPS method towards scalable Li-S battery applications. The tailored pore size which is obtained through increasing CMC content, together with increased  $-\text{COO}^-$  negative groups synergistically suppress the shuttle effect of polysulfides in cells with PC15 separator. On the other hand, the high  $\text{Li}^+$  transference number and lithiophilic oxygen groups promote the uniform Li



stripping/plating even at high current densities and achieve the long-life cycle with a smaller overpotential. As a result, the Li-S battery assembled with PC15 separator displays a high initial discharge capacity of 1392 mAh g<sup>-1</sup> at 0.1 C, an outstanding rate capability of 523.6 mAh g<sup>-1</sup> at 5 C, and a reversible capacity of 520.9 mAh g<sup>-1</sup> after 500 cycles at 1 C with a prominent capacity retention of 0.045% per cycle. This concept from the content tuning of CMC in PVA/CMC composite separators paves a simple and efficient pathway toward low-cost, scalable and ultra-stable advanced Li-S batteries.

#### CRedit authorship contribution statement

**Yuyang Chen:** Conceptualization, Methodology, Investigation, Formal analysis, Data curation, Visualization, Writing – original draft, Writing – review & editing. **Gangyong Zhou:** Investigation. **Wei Zong:** Investigation. **Yue Ouyang:** Investigation. **Kai Chen:** Investigation. **Yan Lv:** Writing – review & editing, Supervision, Funding acquisition. **Yue-Miao:** Writing – review & editing, Supervision, Funding acquisition. **Tianxi Liu:** Writing – review & editing, Supervision, Funding acquisition.

#### Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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#### Appendix A. Supplementary data

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